(19) World Intellectual Property Organization

International Bureau



(43) International Publication Date 8 January 2004 (08.01.2004)

PCT

(10) International Publication Number WO 2004/002620 A1

(51) International Patent Classification⁷: 21/04, 21/10, 23/06, 23/10, 29/06

B01J 21/16,

0, (74)

(21) International Application Number:

PCT/EP2003/006647

(22) International Filing Date:

24 June 2003 (24.06.2003)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

60/392,576

28 June 2002 (28.06.2002) US

02078742.0

4 September 2002 (04.09.2002) H

(71) Applicant: AKZO NOBEL N.V. [NL/NL]; Velperweg 76, 6824 BM Arnhem (NL).

(72) Inventors: O'CONNOR, Paul; Hogebrinkerweg 9, NL-3871 KM Hoevelaken (NL). PEARSON, Gregory, A.; 1211 Goldendale Drive, Seabrook, TX 77586 (US). SPRINGS, Jerry, J.; 605 Canyon Crest, League City, TX 77573 (US). STAMIRES, Dennis; 1300 Colony Plaza, Newport Beach, CA 92660 (US).

(74) Agent: SCHALKWIJK, Pieter, Cornelis; Akzo Nobel N.V., Intellectual Property Deptartment (Dept. AIP), P.O. Box 9300, NL-6800 SB Arnhem (NL).

(81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VC, VN, YU, ZA, ZM, ZW.

(84) Designated States (regional): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE, SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

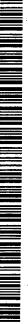
Published:

with international search report

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: FCC CATALYST FOR REDUCING THE SULFUR CONTENT IN GASOLINE AND DIESEL

(57) Abstract: Catalyst composition comprising 5-55 wt% metal-doped anionic clay, 10-50 wt% zeolite, 5-40 wt% matrix alumina, 0-10 wt% silica, 0-10 wt% of other ingredients, and balance kaolin. In metal-doped anionic clays, the additive, i.e. the metal dopant, is distributed more homogeneously within the anionic clay than in impregnated anionic clays, without separate phases of additive being present. Hence, abrasion of this catalyst composition will result in microfines poorer in additive than the prior art composition. Furthermore, the catalyst composition according to the invention results in a higher reduction of sulfur in fuels such as gasoline and diesel than is the case in compositions comprising impregnated anionic clay.



04/002620 A1

FCC CATALYST FOR REDUCING THE SULFUR CONTENT IN GASOLINE AND DIESEL

The present invention relates to a catalyst composition comprising zeolite, alumina, anionic clay, and kaolin, its preparation, and its use in FCC.

Environmental concerns have resulted in legislation limiting the sulfur content in fuels, such as gasoline and diesel. Sulfur, when present in gasoline, not only contributes to SOx-emissions, but also poisons car engine exhaust catalysts.

One way of reducing these sulfur levels is hydrotreating. However, such a process requires substantial capital investments and operating costs. It would be more desirable to reduce the sulfur content in situ, i.e. during processing in the FCC-unit.

WO 99/49001 and T. Myrstad et al., Appl. catal. A 187 (1999) 207-212 disclose such an in situ process using a composition comprising a hydrotalcite material impregnated with a metal additive, i.e. a Lewis acid, preferably Zn. According to this document, the impregnated hydrotalcite material can be incorporated into the matrix of an FCC catalyst, or can be used as a separate compound next to an FCC catalyst.

20

30

5

10

15

Impregnation generally leads to (a) an inhomogeneous distribution of the metal additive in the hydrotalcite material whereby the metal is mainly deposited on the outer surface of the hydrotalcite particles and/or (b) precipitation of the metal additive as a separate phase next to the hydrotalcite material.

25 The so-obtained metal distribution facilitates leaching of the metal additive into the aqueous suspension containing the other catalyst ingredients during the preparation of the catalyst composition. Such leaching leads to a decrease in metal content of the anionic clays (with consequently a loss in catalytic activity) and may result in precipitation of the metal additive on one of the other catalyst ingredients present in the suspension, e.g. the alumina. The presence of such

15

30

metal-containing alumina in the catalyst composition can lead to several side reactions (e.g. coke formation) during use in FCC.

During use of the catalyst composition - which consequently leads to abrasion 5 of the catalyst composition - microfines (dust) are formed. If the metal additive is located mainly on the outer surface of the anionic clay phase and/or if the additive is present as a separate phase within the catalyst, the microfines will contain relatively large amounts of the metal additive. This is environmentally undesired, especially when the additive is a heavy metal-containing compound. Furthermore, with the removal of the metal additive from the catalyst, catalytic activity will be lost.

The present invention provides a catalyst composition comprising 5-55 wt% metal-doped anionic clay, 10-50 wt% zeolite, 5-40 wt% matrix alumina, 0-10 wt% silica, 0-10 wt% of other ingredients, and balance kaolin.

Preferably, the composition comprises 10-35 wt% of metal-doped anionic clay. 20-30 wt% of zeolite, 10-30 wt% matrix alumina, 0-10 wt% of silica, 0-10 wt% of other ingredients, and balance kaolin.

In this specification, the term "metal-doped anionic clay" refers to an anionic 20 clay not containing a binder material, which anionic clay has been formed in the presence of an additive (the dopant). The anionic clay has been prepared by (a) aging an aqueous suspension comprising a divalent metal source and a trivalent metal source, at least one of them being water-insoluble, to form an 25 anionic clay, and optionally (b) thermally treating the anionic clay obtained from step (a) and rehydrating the thermally treated anionic clay to form an anionic clay again.

In metal-doped anionic clays, the metal additive, i.e. the metal dopant, is distributed homogeneously within the anionic clay, without separate phases of metal being present. Hence, microfines resulting from abrasion of this catalyst composition will contain less of the metal additive than microfines resulting from the prior art catalyst composition. Furthermore, less metal will leach out from these doped anionic clays during catalyst preparation than from impregnated anionic clays.

5

The alumina serves as matrix material. This means that the alumina is present in the continuous phase, while the metal-doped anionic clay is present in the discontinuous phase. The difference between the continuous and the discontinuous phase is illustrated in Figure 1.

This situation is opposite to that of WO 01/12570, which discloses an anionic clay-containing shaped body in which the anionic clay constitutes the continuous phase, while the binder material (e.g. alumina) is present in the discontinuous phase. In these shaped bodies it is the anionic clay which serves as matrix material. Such bodies can only be prepared from anionic clay that has good binding properties.

Most anionic clays, however, have poor binding properties. As in the catalyst composition according to the present invention alumina serves as matrix material, this offers the possibility of using any type of anionic clay, either binding or non-binding.

20

25

30

The fact that alumina serves as matrix material does not exclude other binding materials, e.g. silica and/or kaolin, from serving as matrix material as well.

It has been found that the use of catalyst compositions according to the invention results in a higher reduction of the sulfur content in fuels (e.g. gasoline and diesel) than the use of compositions comprising impregnated anionic clay in accordance with WO 99/49001.

The catalyst composition according to the invention can be prepared by mixing zeolite, metal-doped anionic clay, alumina, kaolin, and the optional silica in an aqueous suspension, followed by shaping the material to form particles. The pH

10

15

25

30

of the suspension preferably is between 4 and 8, more preferably between 5 and 7.

Suitable shaping methods include spray-drying, granulation, beading, or any other shaping method suitable for the preparation of FCC catalysts. The amount of liquid present in the precursor mixture used for shaping should be adapted to the specific shaping step to be conducted. It might be advisable to (partially) remove the liquid used in the precursor mixture and/or add additional or other liquid, and/or change the pH of the precursor mixture to make the precursor mixture gellable and thus suitable for shaping. Various additives commonly used in the various shaping methods such as extrusion additives, binders, and fillers may be added to the precursor mixture used for shaping.

Other ingredients, such as metal traps or combustion promoters, pore regulating agents, cationic clays, and other known additives used in FCC catalyst preparation including phosphates may be added to the aqueous suspension mentioned above, or they may be impregnated on the shaped catalyst composition.

The final catalyst particles preferably have an average particle size of 50-100 microns, which makes them suitable for use in FCC units.

20 Metal-doped anionic clay

Anionic clays have a crystal structure which consists of positively charged layers built up of specific combinations of divalent and trivalent metal hydroxides between which there are anions and water molecules. Hydrotalcite is an example of a naturally occurring anionic clay wherein Mg is the divalent metal, Al is the trivalent metal, and carbonate is the predominant anion present. Meixnerite is an anionic clay wherein Mg is the divalent metal, Al is the trivalent metal, and hydroxyl is the predominant anion present.

A variety of terms is used to describe the material that is referred to in this specification as an anionic clay, such as hydrotalcite-like material and layered double hydroxide. In this specification we refer to these materials as anionic

25

clays, comprising within that term hydrotalcite-like materials and layered double hydroxides.

The difference between impregnated and doped anionic clays is that doped anionic clays are prepared by a process wherein the metal additive(s) (hereinafter referred to as metal dopant(s)) is/are present during the formation of the anionic clay, whereas impregnation is always performed after the formation of anionic clay has been completed.

The preparation of metal-doped anionic clay involves aging an aqueous suspension comprising a divalent metal source and a trivalent metal source, at least one of them being water-insoluble. If so desired, the formed anionic clay may be thermally treated (calcined) and then rehydrated to form an anionic clay again.

The dopant(s) is/are introduced in any one of these process steps, e.g. before or during aging or, if a rehydration step is performed, before or during rehydration. A combination of various addition moments can also be applied.

The dopant(s) can be added to the aging suspension either separately or as already present in the insoluble divalent and/or trivalent metal source. In the latter case use is made of a metal-doped divalent and/or trivalent metal source.

The term aging refers to treatment of the suspension at thermal or hydrothermal conditions for 30 minutes to 3 days. In this context, hydrothermal conditions mean in the presence of water (or steam) at temperatures above 100°C and pressures above atmospheric, e.g. autogeneous pressure. Thermal conditions refer to temperatures between 15 and 100°C and atmospheric pressure.

The preparation of metal-doped anionic clay can be conducted batch-wise or in a continuous mode, optionally in a continuous multi-step operation. The process can also be conducted partly batch-wise and partly continuously.

During this process, acids or bases can be added, for example to control the pH.

If an excess of divalent and/or trivalent metal source is present during aging, compositions of anionic clay and unreacted (meaning: not reacted to anionic clay) divalent and/or trivalent metal source can be formed. Such compositions can for instance comprise Mg-Al anionic clay and boehmite and/or brucite. These compositions can suitably be used in the catalyst composition according to the invention.

10

20

25

30

5

After the aging step, the anionic clay is optionally thermally treated to form a solid solution and/or spinel, followed by rehydration of the solid solution to form an anionic clay again. This thermal treatment and rehydration increase the physical strength of the particles.

The thermal treatment can be conducted in an oxygen-containing atmosphere, in a hydrogen-containing atmosphere, in an inert atmosphere or in steam at temperatures varying from 150° to 900°C for a time ranging from a few minutes to 24 hours.

Rehydration is performed by contacting the thermally treated material with a polar liquid, preferably water, at thermal or hydrothermal conditions, preferably at 60-95°C. As mentioned before, metal dopant(s) can be present in the polar liquid during this rehydration step.

During preparation of anionic clay, irrespective of the preparation method used, the solids involved (e.g. solid trivalent metal source, solid divalent metal source, mixtures thereof) can be milled. In this specification the term "milling" is defined as any method that results in reduction of the particle size. Such a particle size reduction can at the same time result in the formation of reactive surfaces and/or heating of the particles. Instruments that can be used for milling include ball mills, high-shear mixers, colloid mixers, and electrical transducers that can introduce ultrasound waves into a slurry. Low-shear mixing, i.e. stirring that is

performed essentially to keep the ingredients in suspension, is not regarded as "milling". If this milling is performed in suspension, metal dopant(s) can be added during the milling.

It is also possible to mill the formed anionic clay.

5

10

20

25

Suitable trivalent metals for the preparation of metal-doped anionic clays include aluminium, gallium, indium, iron, chromium, vanadium, cobalt, manganese, cerium, niobium, lanthanum, and combinations thereof.

Suitable gallium, indium, iron, chromium, vanadium, cobalt, cerium, niobium, lanthanum, and manganese sources are their respective oxides, hydroxides, carbonates, bicarbonates, hydroxycarbonates, acetates, hydroxyacetates, nitrates, chlorides, chlorohydrates, alkoxides, and clays containing the desired metal.

Suitable aluminium sources include aluminium oxides and hydroxides such as transition alumina, aluminium trihydrate (Bauxite Ore Concentrate, gibbsite, bayerite) and its thermally treated forms (including flash-calcined aluminium trihydrate); sols, amorphous alumina, and (pseudo)boehmite, aluminium-containing clays such as kaolin, sepiolite, and bentonite, modified clays such as metakaolin, and/or alumina salts such as aluminium nitrate, aluminium chloride, aluminium chlorohydrate, and sodium aluminate.

It is noted that a water-insoluble trivalent metal source has to be used if the divalent metal source is water-soluble.

Preferred trivalent metal sources are oxides, hydroxides, carbonates, and hydroxycarbonates, as these materials are relatively inexpensive. Moreover, these materials do not leave anions in the metal-doped anionic clay which either have to be washed out or will be emitted as environmentally harmful gases upon heating.

Suitable divalent metal sources include magnesium, zinc, nickel, copper, iron, cobalt, manganese, calcium, barium, and combinations thereof. Suitable zinc, nickel, copper, iron, cobalt, manganese, calcium, and barium sources are the

respective oxides, hydroxides, carbonates, hydroxycarbonates, bicarbonates, acetates, hydroxyacetates, nitrates, chlorides, and clays containing the desired metal.

Suitable magnesium sources include magnesium oxides or hydroxides such as MgO, Mg(OH)₂, hydromagnesite, magnesium salts such as magnesium acetate, magnesium formate, magnesium (hydroxy) acetate, magnesium carbonate, magnesium hydroxy carbonate, magnesium bicarbonate, magnesium nitrate, and magnesium chloride, and magnesium-containing clays such as dolomite, saponite, and sepiolite.

It is noted that a water-insoluble trivalent metal source has to be used if the divalent metal source is water-soluble.

Preferred divalent metal sources for the preparation of metal-doped anionic clays are oxides, hydroxides, carbonates, hydroxycarbonates, bicarbonates, and (hydroxy)acetates, as these materials are relatively inexpensive. Moreover, these materials do not leave anions in the metal-doped anionic clay which either have to be washed out or will be emitted as environmentally harmful gases upon heating.

As mentioned before, also metal-doped divalent and trivalent metal sources can be used for the preparation of metal-doped anionic clays. Examples of such metal sources are metal-doped (pseudo)boehmite, metal-doped Mg(OH)₂, and metal-doped MgO.

Use can be made of Mg-Al anionic clays, Al-containing non-Mg anionic clays, Mg-containing non-Al anionic clays, or non-Mg non-Al anionic clays.

Preferred anionic clays for the present invention are Mg-Al anionic clays, i.e. those which contain aluminium as the trivalent and magnesium as the divalent metal, having a ratio of divalent to trivalent metal from 0.1 to 10, preferably from 1 to 6, and more preferably from 2 to 4. The most preferred ratio is close to 3.

15

20

25

10

15

Suitable Mg-Al anionic clays preferably have either the conventional 3R₁ stacking or the 3R2 stacking according to WO 01/12550. These two types of anionic clays have a three-layer repeat. They are distinguished from each other by the intensities of the (107) and (108) X-ray reflections. The (107) and (108) reflections are generally positioned close to 45 and 47 degrees 2-theta, respectively. In 3R₂-type anionic clays the (107) reflection is stronger than the (108) reflection, whereas in 3R₁-type anionic clays the (108) reflection is stronger than the (107) reflection. The presence of peaks at 45 and 47 degrees 2-theta with comparable intensity suggests the presence of a mixture of these two types of anionic clay. It is to be understood that the precise 2-theta values for the (107) and (108) reflections will depend on the lattice parameters for the Mg-Al anionic clay. There are more differences in the X-ray diffraction pattern, but these are the best distinguishable reflections, because other compounds which are likely to be present in the Mg-Al anionic clay-like material have hardly any reflections around 45-47° 2-theta. Although boehmite has a weak reflection in that range, its presence can be excluded if its strong reflection between 13 and 15 degrees 2-theta is absent.

3R₂-type anionic clays appear to have a different morphology from 3R₁-type anionic clays. The 3R₂-type anionic clay appears to have a structure with irregular flake-like platelets which are randomly agglomerated. Conventional 3R₁-type anionic clay has regular well-formed layers of platelets which are arranged in the usual bookstack form. For more information about different stacking orders of anionic clays reference may be had to Bookin and Drits, <u>Clay and Clay Minerals</u>, Vol. 41, No.5, pages 551-557 and pages 558-564.

25

30

20

The anionic clay is doped with one or more metal dopants. Preferred metal dopants are compounds of the elements selected from the group of zinc, vanadium, iron, copper, tungsten, molybdenum, cobalt, niobium, nickel, chromium, cobalt, rare earth metals, e.g. lanthanum and/or cerium, and combinations thereof. More preferred elements are zinc, vanadium, iron, tungsten, molybdenum, cerium, and combinations thereof.

15

25

If more than one metal dopant is used, it is preferred to use a combination of a Zn-containing compound and a V-containing compound, a combination of a Zn-containing compound and a W-containing compound, a combination of a Fe-containing compound and a V-containing compound, a combination of a Zn-containing compound, a V-containing compound, and a W-containing compound, a combination of a Fe-containing compound, and a W-containing compound, or a combination of a Mo-containing compound and a W-containing compound.

Suitable compounds containing the desired elements are their nitrates, sulfates, chlorides, formates, acetates, oxalates, alkoxides, carbonates, vanadates, molybdates, borates, phosphates, etc.

The metal dopant(s) is/are preferably present in the anionic clay in amounts of less than 70 wt%, more preferably between 2 and 50 wt%, even more preferably between 2 and 30 wt%, and most preferably between 2 and 20 wt%, calculated as metal oxide and based on the weight of metal-doped anionic clay.

If desired, the metal-doped anionic clay may be subjected to ion-exchange.

Upon ion-exchange the interlayer charge-balancing anions are replaced with other anions. Said other anions are the ones commonly present in anionic clays and include pillaring anions such as V₂O₇⁴⁻, HV₂O₁₂⁴⁻, V₃O₉³⁻, V₁₀O₂₈⁻⁶, Mo₇O₂₄⁶⁻, PW₁₂O₄₀³⁻, B(OH)₄⁻⁷, [B₃O₃(OH)₄], [B₃O₃(OH)₅]²⁻, B₄O₅(OH)₄²⁻, HBO₄²⁻,

HGaO₃²⁻, CrO₄²⁻, Keggin-ions, formate, acetate, phosphates, tungstates, and mixtures thereof. Examples of suitable pillaring anions are given in US 4,774,212, which is included by reference for this purpose. Said ion-exchange can be conducted before or after drying the anionic clay-containing composition formed in the suspension.

Zeolites

Preferred zeolites to be used in the catalyst composition of the present invention are pentasil zeolites (e.g. ZSM-5, zeolite beta) optionally containing phosphate, rare earth metal(s) (e.g. RE-ZSM-5), and/or transition metal(s) such as Fe , V, and Zn, and/or faujasite zeolites (e.g. zeolite X, Y, LZ-210), optionally ultrastabilised (USY), dealuminated, and/or exchanged with alkaline earth metals, transition metals, and/or rare earth metals. The preferred zeolite is a rare earth-exchanged zeolite Y or USY with a SAR between 4.0 and 6.0, preferably between 5.0 and 6.0.

10

5

Alumina

Suitable aluminas or alumina sources for the present invention include pseudoboehmite, alumina gel, alumina sol, aluminium chlorohydrol, or aluminium nitrohydrol. The alumina may be peptised with (in)organic acids.

15

20

30

Silica

The composition optionally contains silica. Suitable silica sources are silica gels, silica sols, and Si-Al co-gels. A preferred silica source is silica hydrosol. Silica hydrosols can be prepared by neutralisation of an acidic sodium silicate solution or by ion-exchange of sodium silicate.

The presence of silica is especially preferred if pseudoboehmite is used as matrix material.

Kaolin

The term "kaolin" includes any form of kaolin, such as metakaolin, calcined kaolin, leached kaolin, dealuminated kaolin, etc.

Other ingredients

The composition may also contain other ingredients frequently used in FCC catalysts, such as metal traps, CO combustion promotors, etc. Examples of such other ingredients include alumina-titania, titania, zirconia, cationic clay,

alkaline earth metal (hydr)oxides, borates, phosphates, aluminium phosphates, palladium, and platinum.

The term "cationic clay" includes smectites (e.g. saponite, montmorillonite, bentonite, laponite, hectorite), phosphated smectites, calcined smectites, leached smectites and/or dealuminated smectites.

The catalyst composition is suitable for the production of fuels, such as gasoline and diesel, with relatively low sulfur and nitrogen content. The catalyst composition is especially suitable for the production of said fuels from resid-containing oil feeds.

Figures

5

10

- Figure 1 illustrates a catalyst particle (1) having a continuous phase (2) and a discontinuous phase (3).
- Figure 2 shows an X-ray diffraction pattern of a non-doped, non-impregnated anionic clay.
 - Figure 3 shows an X-ray diffraction pattern of a Zn-impregnated anionic clay. Figure 4 shows an X-ray diffraction pattern of a Zn-doped anionic clay, whereby

the Zn was introduced during rehydration.

- Figure 5 shows an X-ray diffraction pattern of a Zn-doped anionic clay, whereby the Zn was present during aging.
 - Figure 6 shows an electron microscopy photograph of a Ce-impregnated anionic clay.
 - Figure 7 shows an electron microscopy photograph of a Ce-doped anionic clay.

EXAMPLES

Comparative Example 1

An anionic clay was prepared by suspending 1,250 g MgO and 1,210 g flash-calcined gibbsite (Alcoa CP-3®) in 7,540 g water. This mixture was aged at 170°C for 1 hour under autogeneous pressure. The suspension was filtered and the product was dried at 120°C.

The X-ray diffraction pattern of the resulting non-doped, non-impregnated Mg-Al anionic clay is presented in Figure 2.

10

5

A catalyst was prepared by slurrying 10 wt% (on dry base) of the anionic clay with 25 wt% RE-USY zeolite, 30 wt% of a pseudoboehmite peptized with 0.15 mol HNO₃ per mol of Al₂O₃, 5 wt% silicasol, and balance kaolin, followed by spray-drying.

15

20

25

30

Comparative Example 2

An anionic clay was prepared according to Comparative Example 1, except that the resulting anionic clay was impregnated with an aqueous solution of zinc nitrate, using pore volume impregnation. The resulting product had a Zn-content, calculated as ZnO, of 3.5 wt%, and is representative of the prior art WO 99/49001.

The X-ray diffraction pattern of the resulting Zn-impregnated Mg-Al anionic clay is presented in Figure 3. This pattern shows, compared to the pattern of non-doped and non-impregnated anionic clay (Figure 1), additional reflections at about 31.8, 34.4, 36.3, and 56.6 degrees 2-theta (indicated by: *). These additional reflections indicate the presence of a separate ZnO-phase.

A catalyst was prepared by slurrying 10 wt% (on dry base) of the Zn-impregnated anionic clay with 25 wt% RE-USY zeolite, 30 wt% of a pseudoboehmite peptized with 0.15 mol HNO₃ per mol of Al₂O₃, 5 wt% silicasol, and balance kaolin, followed by spray-drying.

Example 3

An anionic clay was prepared according to Comparative Example 1, except that the anionic clay was calcined and subsequently rehydrated in the presence of zinc nitrate. The resulting doped anionic clay had a Zn-content, calculated as ZnO, of 3.5 wt%.

The X-ray diffraction pattern of the resulting Zn-doped Mg-Al anionic clay is presented in Figure 4. It is clear that the separate ZnO-phase which was present in the Zn-impregnated anionic clay of Comparative Example 2 (Figure 2) is not present in this Zn-doped anionic clay. The diffraction pattern of the Zn-doped anionic clay is equivalent to the diffraction pattern of the non-doped non-impregnated anionic clay of Figure 2, indicating a more homogeneous distribution of the Zn-phase within the doped anionic clay compared to the impregnated anionic clay of Comparative Example 2.

15

10

A catalyst was prepared by slurrying 10 wt% (on dry base) of the Zn-doped anionic clay with 25 wt% RE-USY zeolite, 30 wt% of a pseudoboehmite peptized with 0.15 mol HNO₃ per mol of Al₂O₃, 5 wt% silicasol, and balance kaolin, followed by spray-drying.

20

25

30

Example 4

An anionic clay was prepared by suspending 1,190 g MgO, 800 g FC-BOC (Alcoa CP-3®), and 300 g Zn(NO₃)₂.6H₂O in 7,500 g water. This mixture was aged at 170°C under autogeneous pressure for 1 hour. The suspension was filtered and the product was dried at 120°C. The resulting doped anionic clay had a Zn-content, calculated as ZnO, of 4 wt%.

The X-ray diffraction pattern of the resulting Zn-doped Mg-Al anionic clay is presented in Figure 5. This pattern indicates the presence of anionic clay, boehmite, and brucite (Mg(OH)₂). A separate ZnO-phase was not detected, as indicated by the absence of reflection at 31.8, 34.4, 36.3, and 56.6 degrees 2-

theta. Hence, also this way of doping leads to a more homogeneous distribution of the Zn-phase within the product than impregnation.

A catalyst was prepared by slurrying 10 wt% (on dry base) of the Zn-doped anionic clay with 25 wt% RE-USY zeolite, 30 wt% of a pseudoboehmite peptized with 0.15 mol HNO₃ per mol of Al₂O₃, 5 wt% silicasol, and balance kaolin, followed by spray-drying.

Comparative Example 5

10 An anionic clay was prepared according to Comparative Example 1, except that the resulting anionic clay was impregnated with an aqueous solution of cerium nitrate, using pore volume impregnation. The resulting product had a Cecontent, calculated as CeO, of 11 wt%.

Figure 6 presents an electron microscopy photograph of this Ce-impregnated Mg-Al anionic clay, with the Ce-distribution indicated in white. It is clear the Ce is not homogeneously distributed in the anionic clay particles, but is mainly present on the exterior of the particles.

Example 6

15

A Ce-doped anionic clay was prepared according to the method of Example 4, except that zinc nitrate was replaced by cerium nitrate. Figure 7 presents an electron microscopy photograph of this Ce-doped Mg-Al anionic clay, with the Ce-distribution indicated in white. It is clear the Ce in this clay is more homogeneously distributed that in the Ce-impregnated anionic clay of Comparative Example 5.

Example 7

30

The catalyst compositions according to Example 4 and Comparative Examples 1 and 2 were tested in an FCC unit. The sulfur concentration in the resulting gasoline at 65 wt% conversion amounted to 1,434, 1,759, and 1,735 ppmw, respectively. Hence, the use of a Zn-doped anionic clay resulted in a sulfur

reduction which was 17% higher than the sulfur reduction resulting from the use of a Zn-impregnated anionic clay.

CLAIMS

5

10

15

20

25

30

- Catalyst composition comprising 5-55 wt% metal-doped anionic clay, 10-50 wt% zeolite, 5-40 wt% alumina matrix, 0-10 wt% silica, 0-10 wt% of other ingredients, and balance kaolin.
- 2. Catalyst composition according to claim 1 wherein the anionic clay is doped with at least one compound containing an element selected from the group of Zn, Fe, V, Cu, W, Mo, Co, Nb, Ni, Cr, Ce, and La.

 Catalyst composition according to any one of the preceding claims wherein the anionic clay is an Al-Mg-containing anionic clay, an Al-containing non-Mg anionic clay, a Mg-containing non-Al anionic clay, or a non-Mg non-Al anionic clay.

4. Process for the preparation of a catalyst composition according to any one of the preceding claims wherein zeolite, metal-doped anionic clay, alumina, kaolin, and optionally silica and other ingredients are mixed in aqueous suspension and subsequently shaped to form particles.

5. Process according to claim 4 wherein the metal-doped anionic clay is obtainable by mixing a trivalent metal source and a divalent metal source, at least one of them being water-insoluble, in aqueous suspension and aging the mixture in the presence of at least one metal dopant.

6. Process according to claim 4 wherein the metal-doped anionic clay is obtainable by aging a trivalent metal source and a divalent metal source, at least one of them being water-insoluble, in aqueous suspension to form an anionic clay, thermally treating the anionic clay to form a solid solution, and rehydrating the solid solution in the presence of at least one metal dopant to form a metal-doped anionic clay.

5 .

10

15

18

E. L. B. Bull. Annay uniques

- 7. Process according to any one of claims 5-6 wherein the trivalent metal is selected from the group consisting of aluminium, gallium, indium, iron, chromium, vanadium, cobalt, manganese, cerium, niobium, lanthanum, and combinations thereof.
- 8. Process according to any one of claims 5-7 wherein the divalent metal is selected from the group consisting of magnesium, zinc, nickel, copper, iron, cobalt, manganese, calcium, barium, and combinations thereof.
- 9. Process according to claim 7 or 8 wherein the divalent metal source and/or the trivalent metal source are selected from the group consisting of oxides, hydroxides, carbonates, hydroxycarbonates, bicarbonates, acetates, and hydroxyacetates.
 - 10. Process according to any one of the claims 5-9, wherein use is made of a metal-doped divalent and/or metal-doped trivalent metal source.
- 11. Use of a catalyst composition according to any one of claims 1-3 for the production of gasoline and/or diesel having a reduced sulfur content and/or a reduced nitrogen content.

Figure 1

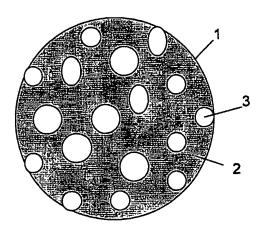


Figure 2

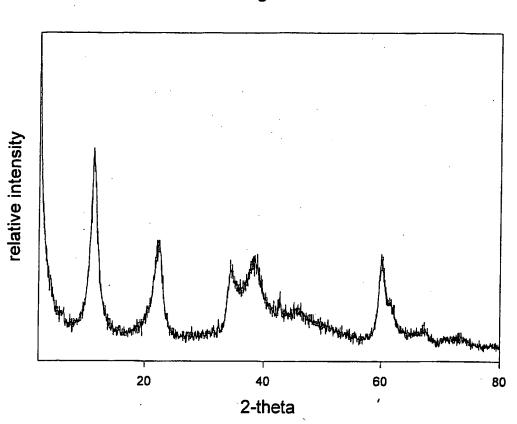


Figure 3

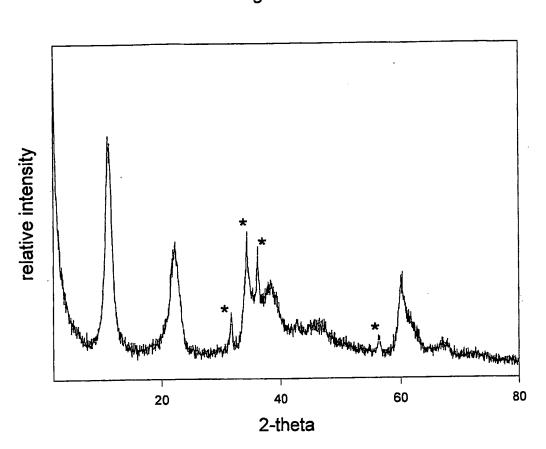


Figure 4

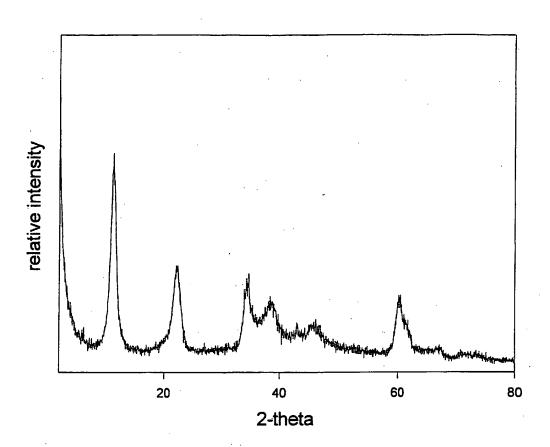


Figure 5

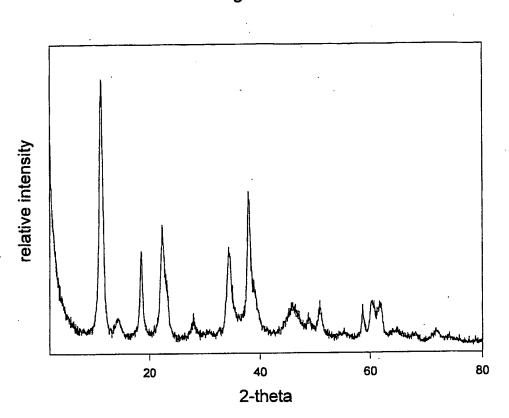


Figure 6.

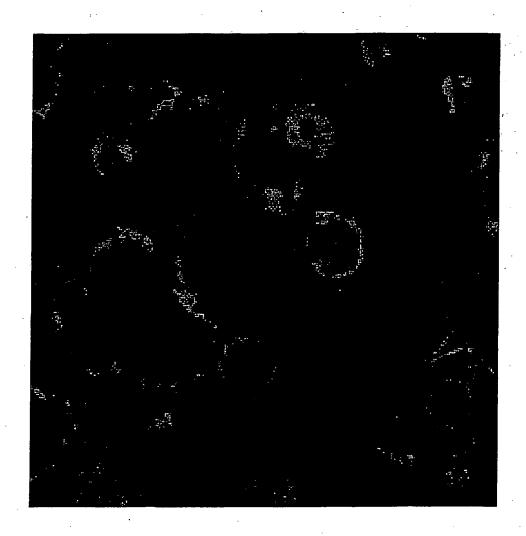
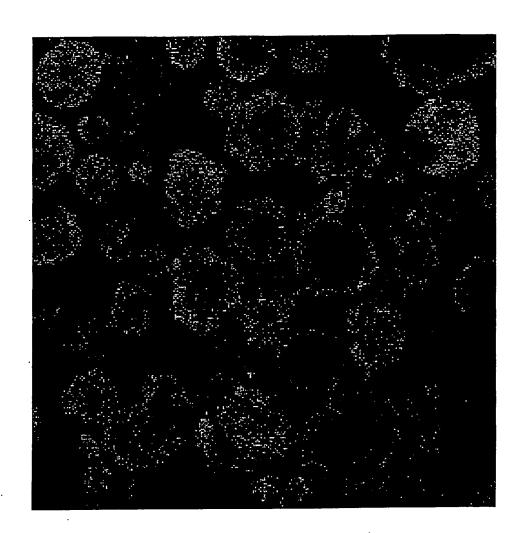


Figure 7



A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 B01J21/16 B01J21/04 B01J21/10 B01J23/06 B01J23/10
B01J29/06

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols) $IPC \ 7 \ B01J$

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 278 535 A (AKZO NV) 17 August 1988 (1988-08-17) page 3, line 26 - line 57 page 4, line 8 - line 33 page 4, line 49 - line 57 page 5, line 5 - line 10 page 5, line 34 - line 56 page 6, line 46 -page 7, line 10 examples 1,6-8	1–11
X	WO 01 12570 A (AKZO NOBEL NV) 22 February 2001 (2001-02-22) page 9, line 24 -page 10, line 29 page 12, line 8 - line 9 examples 5,9,13,16,19,20,28,41,42	1-11

X Further documents are listed in the continuation of box C.	Patent family members are listed in annex.
Special categories of cited documents: A' document defining the general state of the art which is not considered to be of particular relevance E' earlier document but published on or after the international filing date L' document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) O' document referring to an oral disclosure, use, exhibition or other means P' document published prior to the international filing date but later than the priority date claimed	 *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art. *&* document member of the same patent family
Date of the actual completion of the international search 26 August 2003	Date of mailing of the international search report 03/09/2003
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	Authorized officer Schoofs, B

	TO DE DEL SUANT	FC1/Er 03/0004/		
	cition) DOCUMENTS CONSIDERED TO BE RELEVANT Citation of document, with indication, where appropriate, of the relevant passages		Relevant to claim No.	
Category °	Citation of document, with indication, where appropriate, or the			
A	US 4 458 026 A (REICHLE WALTER T) 3 July 1984 (1984-07-03) the whole document	•	1–11	
P,A	WO 02 064504 A (AKZO NOBEL NV) 22 August 2002 (2002-08-22) the whole document		1-11	
P,A	WO 02 064499 A (AKZO NOBEL NV) 22 August 2002 (2002-08-22) the whole document	·	1-11	
P,A	WO 02 072474 A (AKZO NOBEL NV) 19 September 2002 (2002-09-19) the whole document		1-11	
		·		
			·	

PUI/EF U3/U664/

Patent document cited in search report		Publication date		Patent family member(s)	Publication date
EP 0278535		17-08-1988	AT	60874 T	15-02-1991
			AU	609763 B2	
		•	AU	1021288 A	14-07-1988
•			BR	8707099 A	02-08-1988
			CA	1314862 C	23-03-1993
•			DE	3861771 D	
	•		ĒΡ	0278535 A	
			GR	3001934 T	
		•	JP	2678276 B2	
			ĴΡ	63182031 A	27-07-1988
			ÜS	4866019 A	12-09-1989
	•		ÜS	4946581 A	07-08-1990
			US	4952382 A	28-08-1990
W0 0112570	A	22-02-2001	BR	0013137 A	30-04-2002
			CA	2381391 A	
			CN	1371341 T	25-09-2002
			WO	0112570 A1	
			EP	1206424 A1	
			JР	2003507303 T	25-02-2003
			US	6589902 B1	
US 4458026	A	03-07-1984	US	4476324 A	09-10-1984
			CA	1203071 A1	15-04-1986
			DE	3371981 D1	16-07-1987
•			ΕP	0095783 A2	2 07-12-1983
			JP	1634409 C	20-01-1992
•			JP	2060376 B	17-12-1990
			JP	58219139 A	20-12-1983
WO 02064504	A	22-08-2002	WO	02064504 A1	22-08-2002
			US	2002159940 A1	31-10-2002
WO 02064499	Α	22-08-2002	WO	02064499 A2	
			US	2002111263 A1	15-08-2002
WO 02072474	Α	19-09-2002	WÓ	02072474 A1	19-09-2002
			US	2002092812 A1	18-07-2002



This Page is Inserted by IFW Indexing and Scanning Operations and is not part of the Official Record

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

BLACK BORDERS

IMAGE CUT OFF AT TOP, BOTTOM OR SIDES

FADED TEXT OR DRAWING

BLURRED OR ILLEGIBLE TEXT OR DRAWING

SKEWED/SLANTED IMAGES

COLOR OR BLACK AND WHITE PHOTOGRAPHS

GRAY SCALE DOCUMENTS

LINES OR MARKS ON ORIGINAL DOCUMENT

REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY

IMAGES ARE BEST AVAILABLE COPY.

☐ OTHER:

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.

